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μ
μ
μ .
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μ .

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	1					10	
1.1.		μ				10	
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7.2.		μ	153
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			155
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			159
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			161
			165

1.1.2. μ μ

μ μ μ μ μ , μ (test)
 μ μ . μ
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2 100 μ 1 μ ; , test μ
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1. μ μ . μ μ
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μ , μ
μ μ .
μ μ 19 ,
μ **1889**, μ
μ platinum-iridium.

μ μ μ .
1893 μ μ μ μ (μ μ
μ) 1.553.164,13
μ μ μ μ μ , 760mm

μ 15 μ .
μ μ **1960.** 14 , 11
μ (Conférence Générale des Poids et Mesures) μ

1.650.763,73 μ μ μ μ μ

Kr⁸⁶ .

μ μ **1983**, 17 , μ
1/299.792.458

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μ 1.1.

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μ μ μ μ **1975**

μ μ μ

- μ (BIPM).
- μ (CGPM).
- μ (CIPM).

μ	μ		/	μ	μ
yotta	Y		10^{24}	$\mu\mu$	μ
zetta	Z		10^{21}	$\mu\mu$	μ
exa	E		10^{18}	$\mu\mu$	μ
peta	P		10^{15}	$\mu\mu$	μ
tera	T		10^{12}	$\mu\mu$	μ
giga	G		10^9	$\mu\mu$	μ
mega	M	μ	10^6	$\mu\mu$	$\mu \mu$
kilo	k		10^3		μ
hecto	h		10^2		μ
deca	da		10^1		μ
unit	un	μ	$10^0 = 1$	μ	μ
deci	d		10^{-1}		μ
centi	c		10^{-2}		μ
milli	m		10^{-3}		μ
micro	μ	μ	10^{-6}	$\mu\mu$	$\mu \mu$
nano	n		10^{-9}	$\mu\mu$	μ
pico	p		10^{-12}	$\mu\mu$	μ
femto	f	μ	10^{-15}	$\mu\mu$	$\begin{pmatrix} \mu & \mu \\ & \mu \end{pmatrix}$
atto	a		10^{-18}	$\mu\mu$	μ
zepto	z		10^{-21}	$\mu\mu$	μ
yocto	y		10^{-24}	$\mu\mu$	μ

1.2: $\mu \mu$.

_____ μ
 μ , μ , μ .
 μ , μ Heisenberg, μ μ :

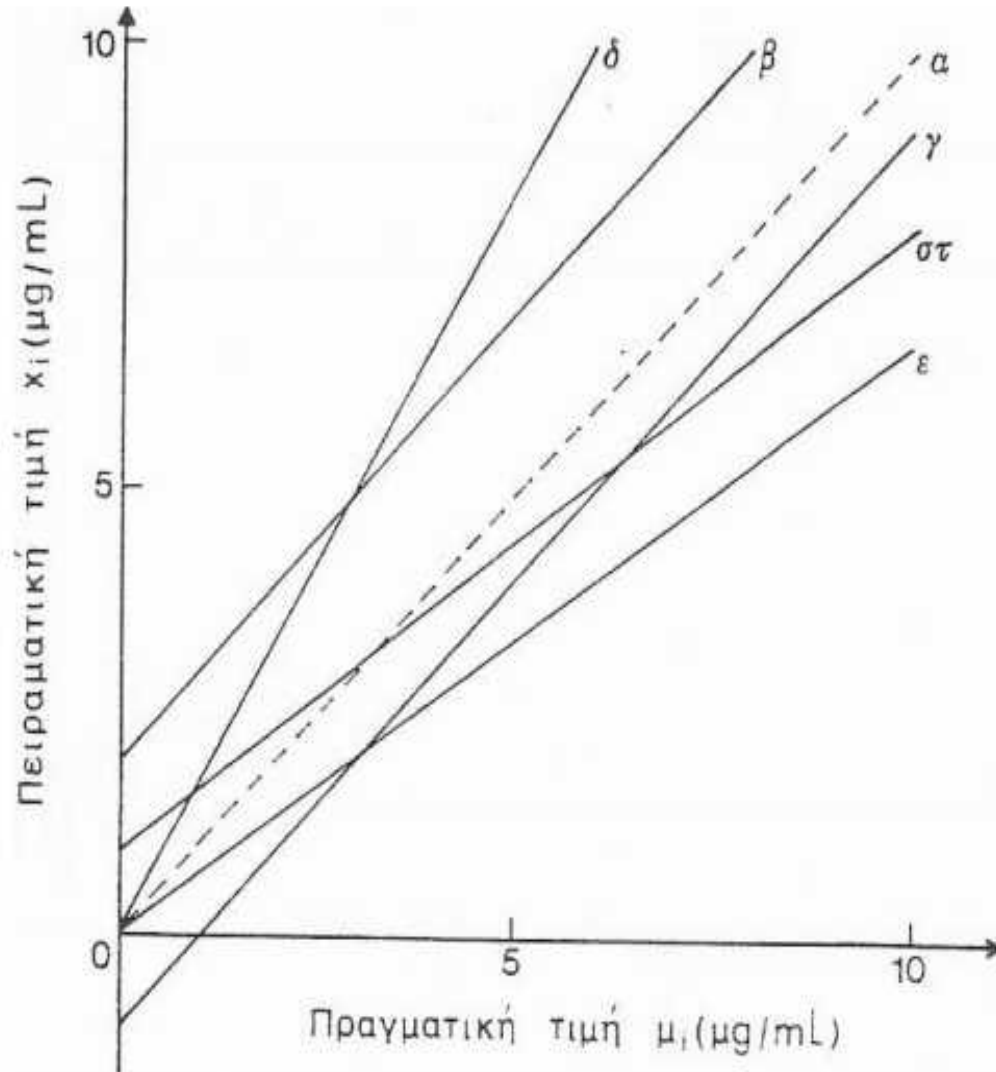
$$\Delta p * \Delta x \geq \frac{h}{2\pi} \quad (1.1)$$

p: μ μ μ
 x: μ μ μ
 h: $6.626176 \cdot 10^{-27}$, Plank.
 μ $\times \mu$ ($\Delta x \rightarrow 0$),
 ($\Delta p \rightarrow \infty$), p .

_____ μ
 « μ » μ μ
 μ , μ μ , μ μ
 , μ , , μ
 μ μ . μ
 μ μ , μ ,
 μ μ μ μ μ μ μ
 μ . μ μ μ :

$$\mu \pm$$

μ
 μ μ μ μ , μ
 μ , =26°C, R = 22.11 kOhm =79°C, R=21.67 kOhm. μ
 μ μ μ μ μ R(), μ
 μ , =26°C, R= (22.11±0.04) kOhm =79°C, R=(21.67±0.04) kOhm.
 μ , μ μ .



μ 2-2. μ μ μ μ μ μ μ μ
 :) μ μ . ,) μ
 +0.2 μ g/mL μ μ ,) μ -1.0 μ g/mL
 μ μ ,) μ +66.7° μ ,) μ -33.3°
 μ) μ +1.0 μ g/mL μ μ
 (μ -30%).

μ , μ μ ,
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2.2.2.

μ μ μ ,
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 μ μ μ μ μ μ μ .
 μ μ .

- μ μ .
- _____ :
- ❖ _____ μ _____ μ μ μ _____ .
 - ❖ _____ μ _____ μ _____ .
- _____ μ _____ μ _____ ,
- μ μ μ μ μ μ μ μ μ μ .
- ❖ _____ μ _____ μ _____ .
- _____ μ _____ μ _____ μ _____ μ _____ .

μ 2^* : $S = 622,60 \text{ m}$ μ $S = \pm$
 20 cm μ $S = 280,70 \text{ m}$ μ $S = \pm 15 \text{ cm.}$ μ
 μ ;

:

$$\frac{\Delta S_1}{S_1} = \frac{\pm 20 \text{ cm}}{62260 \text{ cm}} = \pm 0,00032 = \pm 0,032 \%$$

$$\frac{\Delta S_2}{S_2} = \frac{\pm 15 \text{ cm}}{28070 \text{ cm}} = \pm 0,00053 = \pm 0,053 \%$$

μ μ $\mu \mu$

.

μ μ μ

μ μ μ μ μ μ μ

$\mu \mu$ μ $Y,$ μ

$$Y = f(x_1, x_2, x_3, \dots, x_k)$$

μ x_i μ $x_i,$ μ :

$$= f(x_1, x_2, x_3, \dots, x_k)$$

μ μ μ μ μ μ

μ , μ ϵ_ψ .

μ μ μ

:

$$d_\psi = \frac{\theta_\psi}{\theta x_1} \cdot dx_1 + \frac{\theta_\psi}{\theta x_2} \cdot dx_2 + \dots + \frac{\theta_\psi}{\theta x_k} \cdot dx_k$$

$$dx_i = \epsilon_i, \quad \epsilon_i \quad \mu, \mu \quad :$$

$$d_\psi \approx \Delta_\psi \approx \epsilon_\psi$$

:

$$\varepsilon_{\psi} = \frac{\theta_{\psi}}{\theta x_1} \cdot \varepsilon_1 + \frac{\theta_{\psi}}{\theta x_2} \cdot \varepsilon_2 + \dots + \frac{\theta_{\psi}}{\theta x_{\kappa}} \cdot \varepsilon_{\kappa}$$

$$\varepsilon_1 \quad \mu \quad \mu \quad \Delta x_1$$

μ . μ , μ

μ

$$\Delta \psi_{max} = (\left| \frac{\theta_{\psi}}{\theta x_1} \cdot \Delta x_1 \right| + \left| \frac{\theta_{\psi}}{\theta x_2} \cdot \Delta x_2 \right| + \dots + \left| \frac{\theta_{\psi}}{\theta x_{\kappa}} \cdot \Delta x_{\kappa} \right|)$$

$$= f(x) \quad \mu \quad \mu \quad \mu \quad \mu \quad , \quad x$$

$x \quad \mu$

$$\Delta \psi = f(x) \cdot x$$

μ :

$$\Delta \psi_x = \frac{\Delta \psi_{max}}{\psi}$$

$\mu \quad I$: $\mu \quad \mu \quad R \quad \mu \quad I$

$$= 15 \pm 0,3 \text{ A} \quad U = 110 \pm 2 \text{ V.} \quad \mu \quad \mu$$

R ;

:

$\mu \quad \mu \quad \mu \quad \text{Ohm} \quad \mu$,

$$R = \frac{U}{I} = f(U, I)$$

μ ,

$$\Delta R_{max} = \pm (\left| \frac{\theta_R}{\theta U} \cdot \Delta U \right| + \left| \frac{\theta_R}{\theta I} \cdot \Delta I \right|)$$

$$\Delta R_{max} = \pm (\left| \frac{\Delta U}{I} \right| + \left| \frac{U}{I^2} \cdot \Delta I \right|)$$

μ :

$$\Delta R_r = \frac{\Delta R_{max}}{R} = \pm \frac{2}{110} + \frac{0,3}{15} \approx \pm 0,04$$

118,5 cm μ 2° : μ μ μ μ $l =$
 $T = 2,180 \text{ sec},$ μ $g.$

$$\pm 1 \text{ cm} \cdot \text{sec}^{-2}.$$

:

$$\mu \quad \mu \quad ,$$

:

$$T = 2\pi \cdot \sqrt{\frac{l}{g}}$$

$$g = \frac{4\pi^2 \cdot l}{T^2} = \quad (l, T)$$

$$\Delta g_{max} = \pm \frac{4\pi^2}{T^2} \cdot \Delta l + \frac{-8\pi^2 \cdot l}{T^3} \cdot \Delta T = \pm 1 \text{ cm} \cdot \text{sec}^{-2}$$

$$\mu \quad \mu$$

μ :

$$\frac{4\pi^2}{T^2} \cdot \Delta l = \pm 0,5 \text{ cm} \cdot \text{sec}^{-2}$$

$$\Delta l = \pm \frac{T^2}{4\pi^2} \cdot 0,5 \text{ cm} \cdot \text{sec}^{-2} = 0,06 \text{ cm}$$

$$\frac{8\pi^2 \cdot l}{T^3} \cdot \Delta T = \pm 0,5 \text{ cm} \cdot \text{sec}^{-2}$$

$$\Delta T = \frac{T^3}{8\pi^2 \cdot l} \cdot 0,5 \text{ cm} \cdot \text{sec}^{-2} = \pm 0,00055 \text{ sec}$$

$$d \ln \rho = \frac{d\rho}{\rho} = \frac{dm}{m} - \frac{2dD}{D} - \frac{dh}{h}$$

$$dm = m, \quad d(D) = D \quad dh = h \quad \mu :$$

$$\frac{\Delta \rho_{\max}}{\rho} = \frac{0,1}{970} + \frac{2 \cdot 0,1}{4,84} + \frac{0,01}{6,74} = 0,0057 \approx \pm 0,6 \%$$

$$\mu \quad \mu \quad \mu \quad :$$

$$\frac{\Delta \rho_{\max}}{\rho} = \pm 0,6 \%$$

:

$$\rho = 7,81 \frac{\text{gr}}{\text{cm}^3}$$

$$\mu \quad \mu \quad \mu \quad :$$

$$\Delta \rho_{\max} = \pm 0,0057 \rho = \pm 0,045 \frac{\text{gr}}{\text{cm}^3} \approx 0,05 \frac{\text{gr}}{\text{cm}^3}$$

μ

$$\rho = 7,81 \pm 0,05 \frac{\text{gr}}{\text{cm}^3}$$

2.3.1.

Gauss

Gauss 19

μ μ μ μ μ .

μ μ .

μ , μ n μ , μ

μ μ μ . μ μ $l_1, l_2, l_3, \dots, l_n$.

μ , μ μ , μ

μ μ μ μ . μ

Gauss

 $x \quad \mu \quad \mu \quad x. \quad x$

$$\sum_{i=1}^n U_i^2 = x - l_1^2 + x - l_2^2 + \dots + x - l_n^2 = f(x) \quad (1)$$

 $\mu \quad \mu \quad \mu$

$$\frac{df}{dx} = 2x - l_1 + 2x - l_2 + \dots + 2x - l_n = 0$$

:

$$nx = l_1 + l_2 + \dots + l_n$$

$$x = \frac{\sum l_i}{n} \quad (2)$$

 $\mu \quad x \quad \mu \quad \mu \quad \mu$
 $\mu \quad \mu$
 $U_i \quad \mu \quad l_i \quad \mu \quad \mu$
 μ

$$U_i = x - l_i \quad i = 1, 2, 3, \dots, n \quad (3)$$

 $\mu \quad \mu \quad \mu \quad n$
 $\mu \quad x \quad \mu \quad X.$

$$(3) \quad \mu \quad , \quad (2) \quad :$$

$$\sum u = n \cdot x - \sum l = n \cdot \frac{\sum l}{n} - \sum l = 0 \quad (4)$$

 $\mu \quad \mu \quad \mu \quad \mu \quad \mu \quad \mu$
 $\mu \quad \mu \quad \mu \quad \mu \quad \mu \quad \mu$
 $x_0, \quad \mu \quad x \mu \mu \quad \mu$
 $\mu \quad x_0 \quad \mu \quad x \quad x \mu \quad :$

$$x = x_0 + \delta x$$

 $(3) \quad :$

$$U_i = x_0 + \delta x - l_i = \delta x - (l_i - x_0)$$

 $, \quad \mu \quad \sum (\chi - l_i)_{\epsilon \lambda \alpha \chi}^2 \quad :$

$$\delta_x = \frac{\sum (l - x_0)}{n}$$

$$x = \left(1282.0 + \frac{8,8}{8} \right) mm$$

$$x = 1283,1 mm$$

$$t = \pm \frac{1,6}{8} mm = \pm 0,2 mm$$

$$m = \pm \sqrt{\frac{0,3}{7}} mm = \pm 0,23 mm$$

$$x = \left(1282.0 + \frac{8,8}{0} \right) mm$$

$$x = 1283,0 mm$$

$$t = \pm \frac{1,6}{8} mm = \pm 0,2 mm$$

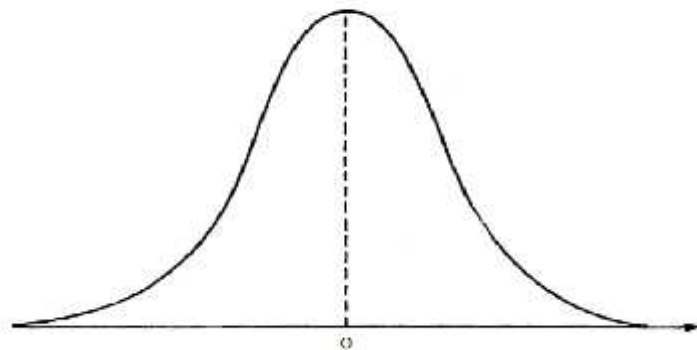
$$m = \pm \sqrt{\frac{0,72}{7}} mm = \pm 0,32 mm$$

μ μ μ μ ,
 μ μ μ .
 μ , μ μ μ μ μ
 μ . μ μ μ
. μ μ U_i μ μ μ ,
 μ μ μ .

2.5.

μ Gauss

μ Gauss μ
 μ μ μ , ,
 μ μ μ μ , μ μ
 μ , μ μ μ μ
 μ μ μ μ
 μ .



$$Q = \frac{\sum(x_1 - \bar{x})^2}{n - 1}$$

μ , $(x_1 - \bar{x})$ μ μ n μ μ .
 μ : μ μ μ μ μ .
 μ , μ μ μ 25,550 ± 0,01 mm.
 μ μ μ .

μ μ	μ	μ μ	μ
1	25,552 mm	6	25,558 mm
2	25,552 mm	7	25,554 mm
3	25,544 mm	8	25,550 mm
4	25,548 mm	9	25,544 mm
5	25,546 mm	10	25,552 mm

μ μ ;
 100.000 μ , ,
 ;
 :

μ μ 25,500 mm μ μ μ . μ

μ	/	x	$x_1 - \bar{x}$		$(x_1 - \bar{x})^2$	
			+	-		
1		52	2		4	$\bar{x} = \frac{\sum x_1}{N} =$ $= \frac{500}{10} = 50$
2		52	2		4	
3		44		6	36	
4		48		2	4	
5		46		4	16	

μ μ μ . μ
 μ , , μ
 .
 μ μ μ
 μ μ μ ,
 , μ , .
 :

I) μ μ μ μ
 μ .

II) μ μ μ μ μ
 , μ ,

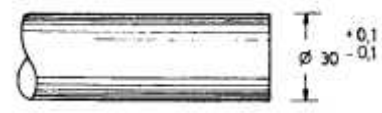
III) μ , μ μ μ ,
 , μ μ μ

IV) μ , μ
 μ .

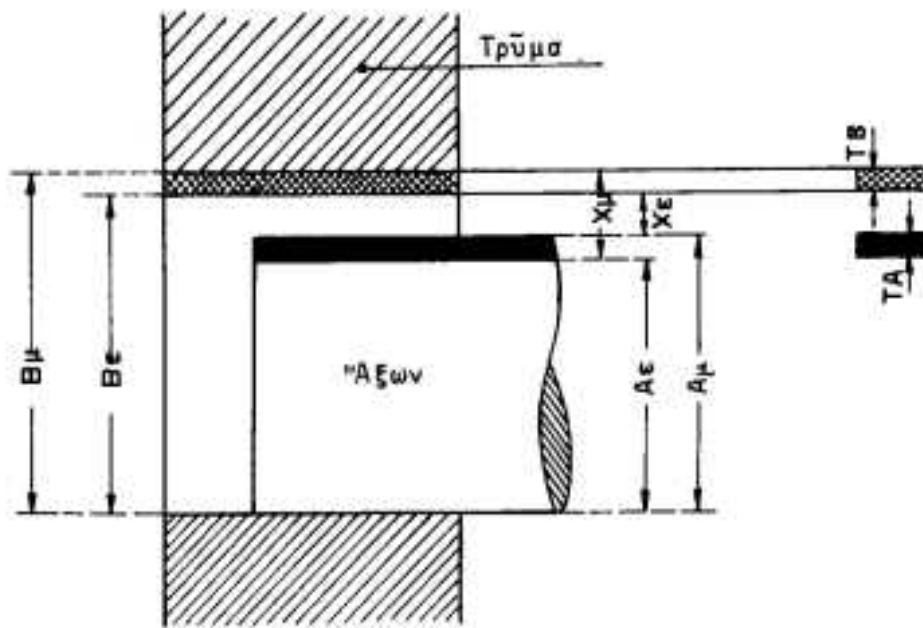
V) μ μ μ .
 μ μ

μ μ μ . μ
 μ μ μ μ . ,
 μ μ μ , .
 μ , , μ ,
 μ , μ μ . μ
 μ μ μ « » .

μ , μ
 μ , μ μ ,



$$X_{\mu} \geq - \geq X_{\varepsilon} \quad (1)$$

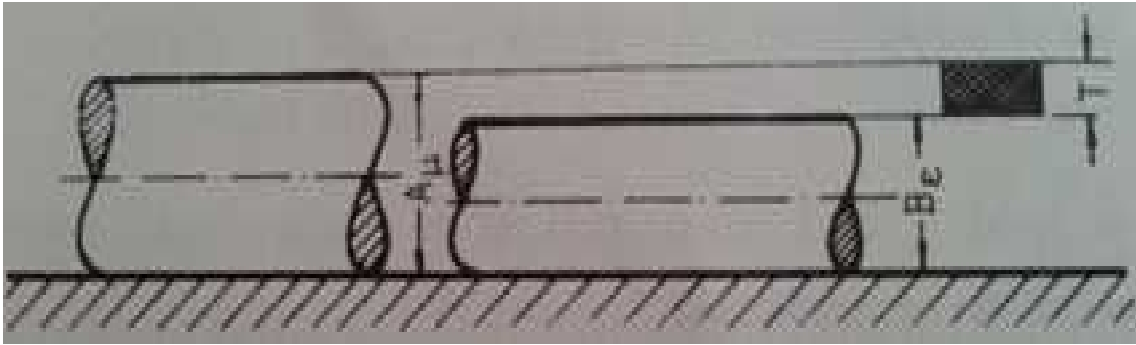


3.1

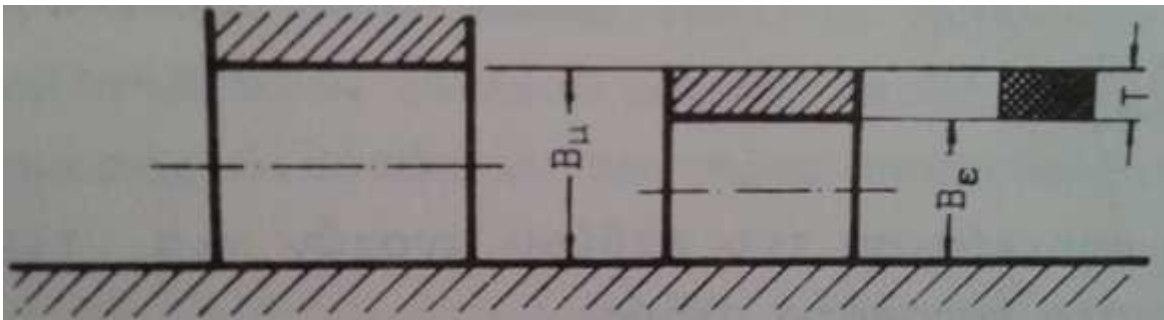
$$X_{\mu} = E_{\mu} - A_{\varepsilon} \quad (2)$$

$$X_{\varepsilon} = E_{\varepsilon} - A_{\mu} \quad (3)$$

μ 10°C. μ μ
 μ μ . μ μ
 μ , μ μ μ .
 μ μ 20°C μ μ μ .
 μ μ μ μ .
 μ μ μ μ μ . μ 20°C μ μ
 μ μ μ μ μ μ .
 μ μ . μ μ μ
 μ μ , μ μ
 μ μ μ , μ μ μ , μ
 μ μ μ μ μ μ .
 μ μ : μ μ μ μ μ . μ
 μ μ : μ μ μ .
 μ : μ (A_μ) (A_ϵ) μ (B_μ)
 (B_ϵ) μ . μ
 μ μ μ μ μ , .
 μ : D_g, L_g μ .
 μ : D_k, L_k μ μ .
 (T_A) μ ($T_B)$ μ μ
 μ .
 μ : $T_A = A_\mu - A_\epsilon$ $T_B = B_\mu - B_\epsilon$.
 μ () : μ μ : $T = T_A + T_B$.

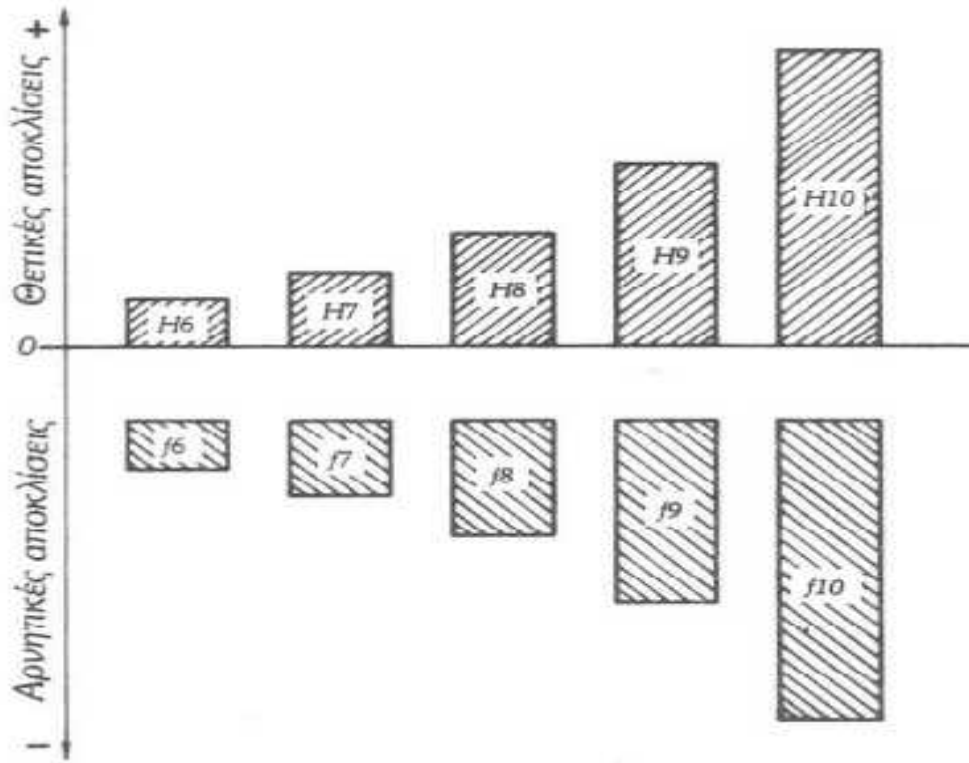


3.2 .:



3.3.: μ

$\mu\mu$: $\mu\mu$
 μ μ μ . μ μ
 μ .
 μ - μ , 27μ , μ 27
 μ . μ μ μ $\mu\mu$.
 μ , μ $\mu\mu$ μ μ ,
 $\mu\mu$.
 μ μ μ , 30 8 ,
 μ , μ 30mm , 8 .



6.4.

μ : μ μ μ μ
 μ μ μ μ μ
 μ μ μ μ μ
 μ μ μ μ μ

μ 80mm

100μm.

1. 80^{+050}_{-050} μμ

2. 80^{+040}_{-060} μμ

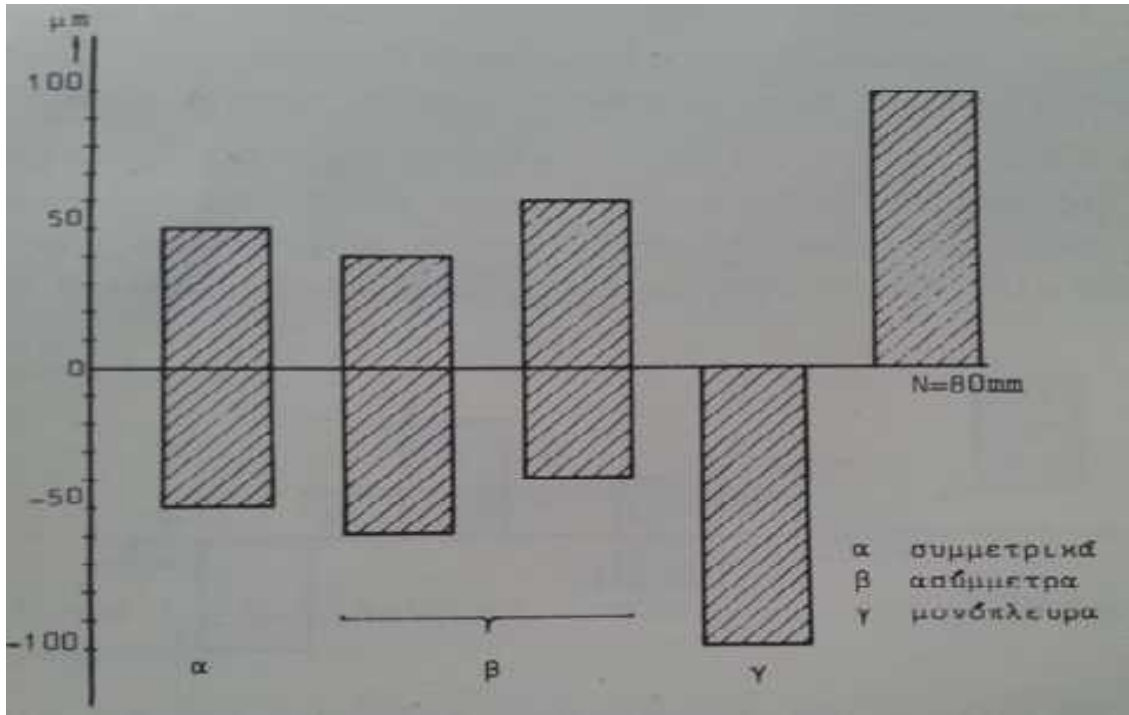
3. 80^{+060}_{-040}

3. 80^{+000}_{-100}

3. 80^{+100}_{-000}

μ .

μ .



6.4.:

μ

μ

μ

:

μ

μ

:

$$A_0 = L_g - N$$

:

$$A_k = L_k - N$$

μ

μ μ

$$A_0 = +46\mu m = 0,046mm$$

$$A_k = 0 mm$$

$$D_g = N + A_0 = 40 + 0.046 = 40.046mm$$

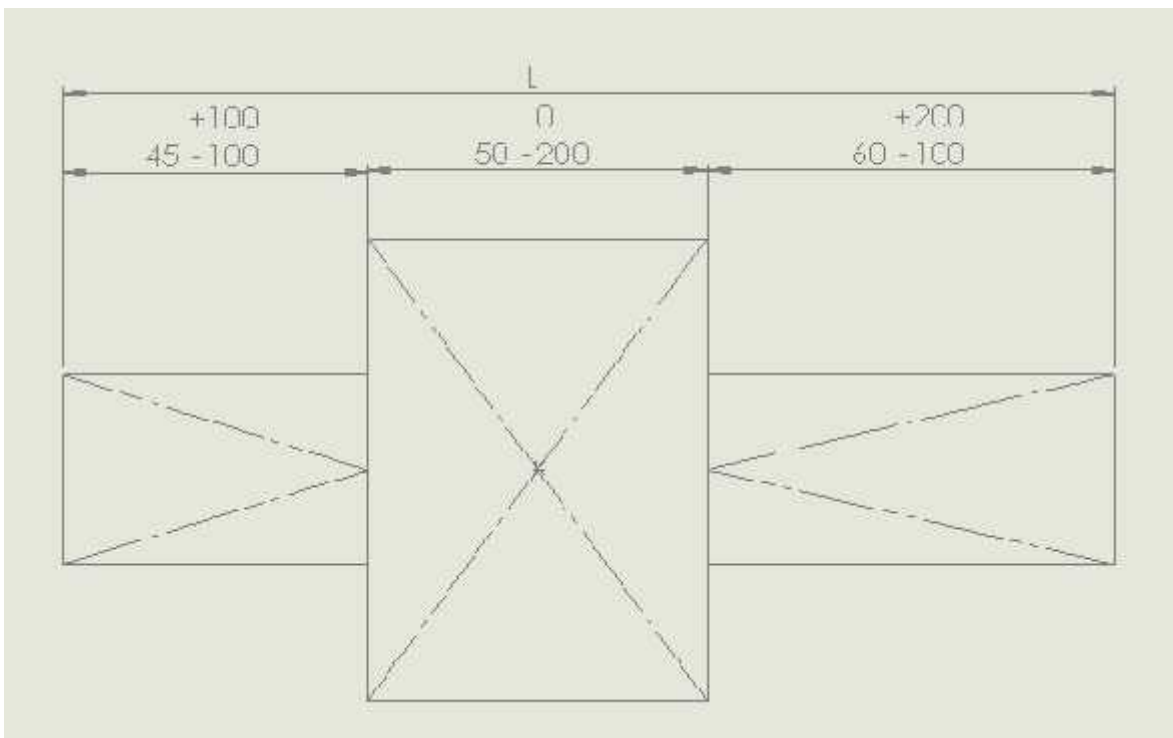
$$D_k = N + A_k = 40 + 0.00 = 40mm$$

$$T_b = D_g - D_k = A_0 - A_k = 40.046 - 40.000 = 0.046mm$$

μ

μ

μ L



$$T_A = A_{\mu} - A_{\epsilon},$$

$$= 45,100 - 44,900 = 0,200 \text{ mm}$$

$$= 50,000 - 49,800 = 0,200 \text{ mm}$$

$$= 50,200 - 59,900 = 0,300 \text{ mm}$$

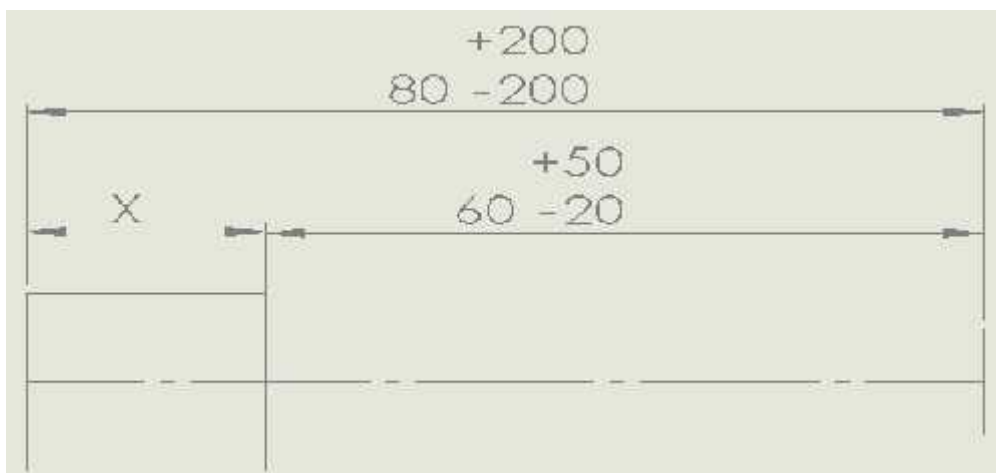
$$L_g = 45.100 + 50.000 + 60.200 = 155.300 \text{ mm}$$

$$L_k = 44.900 + 49.800 + 59.900 = 154.600 \text{ mm}$$

$$L = L_g - L_k = 155.300 - 154.600 = 0.700 \text{ mm}$$

155mm, 300μm, 400μm.
 155^{+300}_{-400}

μ



μ μ μ :

$$X_{max} = 80.200 - 59.80 = 20.220mm$$

$$X_{min} = 79.800 - 60.050 = 19.750mm$$

Δι σταση 80^{+200}

$$= 80.200 - 79.800 = 0.400mm$$

Δι σταση 60_{-20}^{+50}

$$= 60.050 - 59.980 = 0.070mm$$

$$= 80 - 60 = 20 \text{ mm}$$

$$= 0.400 + 0.070 = 0.470mm$$

$$: X_{A_0} = +0.200 - -0.020 = +0.220mm$$

$$: X_{A_K} = -0.020 - +0.50 = -0.250mm$$

3.4.

μ

μ μ μ μ μ μ μ μ ,

μ μ ,

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μ : , , μ

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: μ μ μ μ μ

μ . μ μ ,

μ μ . μ

, , (X_e)

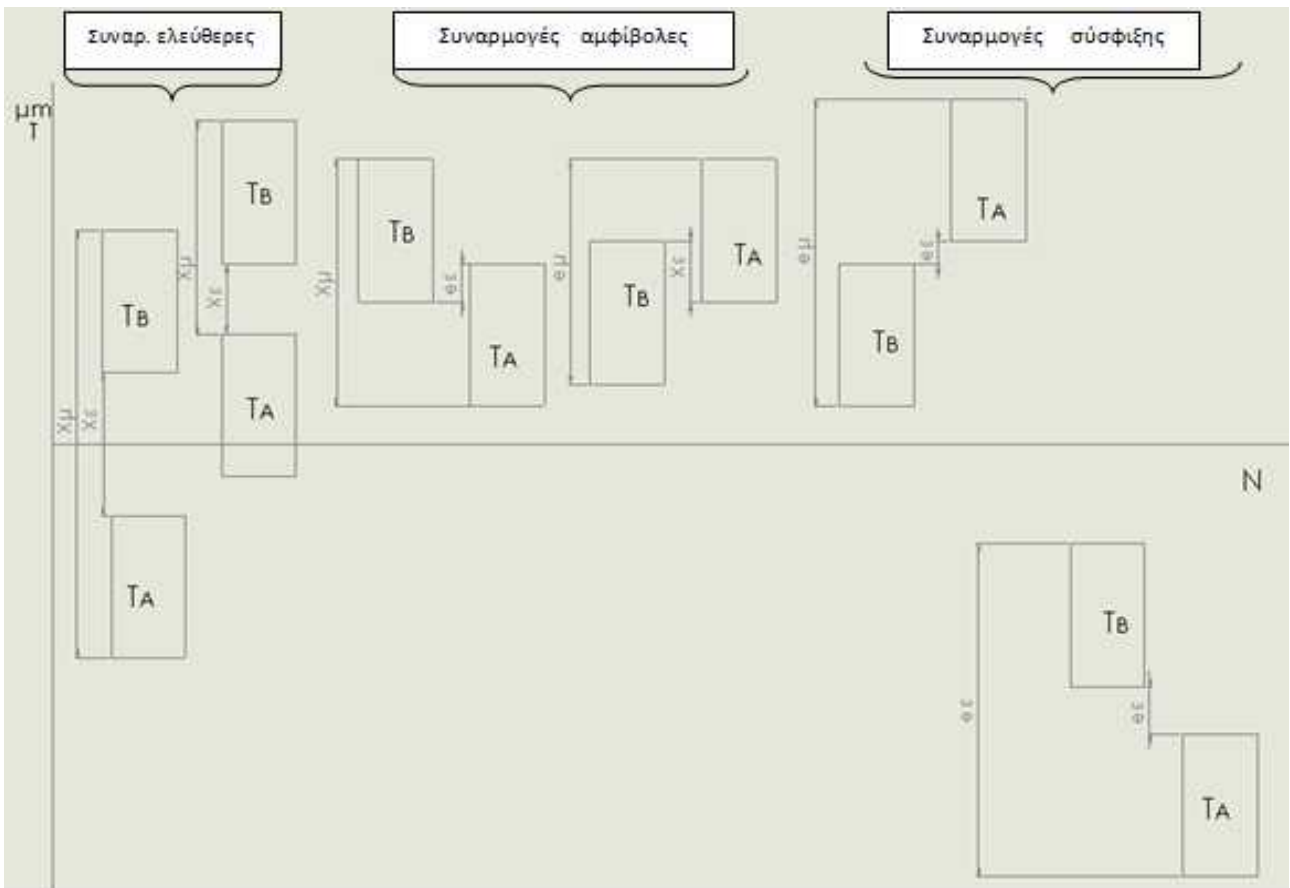
_____ μ :

μ 60_{-40}^{+000} μ μ 60_{+40}^{+80}

:

$$A_\mu = 60,000mm$$

$$E_\mu = 60,080mm$$



3.8.

- i) μ . μ
- ii) μ . μ
- iii) μ , μ . μ μ

3.6 μ ISO

- μ , μ . $\mu\mu$
- μ : μ .
- μ μ 20 C. μ , $\sqrt[3]{D}$.

- μ $\mu\mu$.
- μ μ ().

3.6.1.

μ μ I.S.O. μ $\mu\mu$ i μ
 μ μ :

$$i = 0.45 \sqrt[3]{D} + 0.001 D$$

$D = \mu$ mm

$I = \mu$ μm

$0,001 D$ μ μ μ

3.6.2.

μ μ μ I.S.O. 18 μ μ
 μ 1 22, I.T1 ÷ I.T22 .
 $\mu\mu$. . International Tolerance.

6 μ 10i.

μ μ 1,6.

μ I.T.7 = 1,6 I.T. 6 = 1,6*10i = 16i

μ 6 μ .

μ 1÷500mm 15 μ μ

μ μ μ

μ .

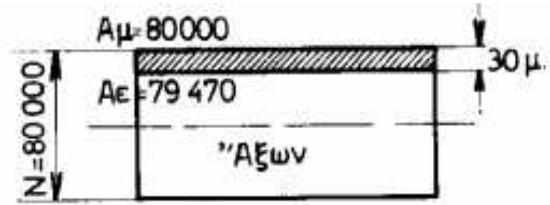
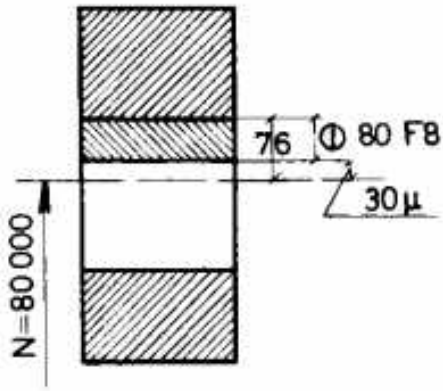
 μ

μ 6 10 mm 6 (I.T.6).

μ μ :

$$D_{\mu} = \sqrt{6 * 10} = \sqrt{60} = 7.75\text{mm}$$

μ D=7.75 mm :



μ - μ ,
 μ μ .
 μ μ - , ,
 μ μ μ .
 μ , μ I.S.O. μ μ .
 μ μ , μ μ h
 μ , μ μ .
 μ μ μ μ μ .

 μ

μ μ $42 \Phi \frac{G6}{h5}$ μ ;

μ μ μ μ I.S.O.

a. μ - μ μ μ 42mm

b. μ

c. μ G.

d. μ 6.

e. h

f. 5.

g. μ μ

μ :

μ $42 \Phi G6$ $42 \Phi \frac{+025}{-009}$

$$42^{\text{H}}_{25} \quad 42^{\text{O}}_{-013}$$

μ :

$$E_{\mu} = 42,025\text{mm} \quad A_{\mu} = 42,000\text{mm}$$

$$E_{\varepsilon} = 42,009\text{mm} \quad A_{\varepsilon} = 41,987\text{mm}$$

μ , μ :

$$X_{\mu} = E_{\mu} - A_{\varepsilon} = 42,025 - 41,987 = 0,038\text{mm}$$

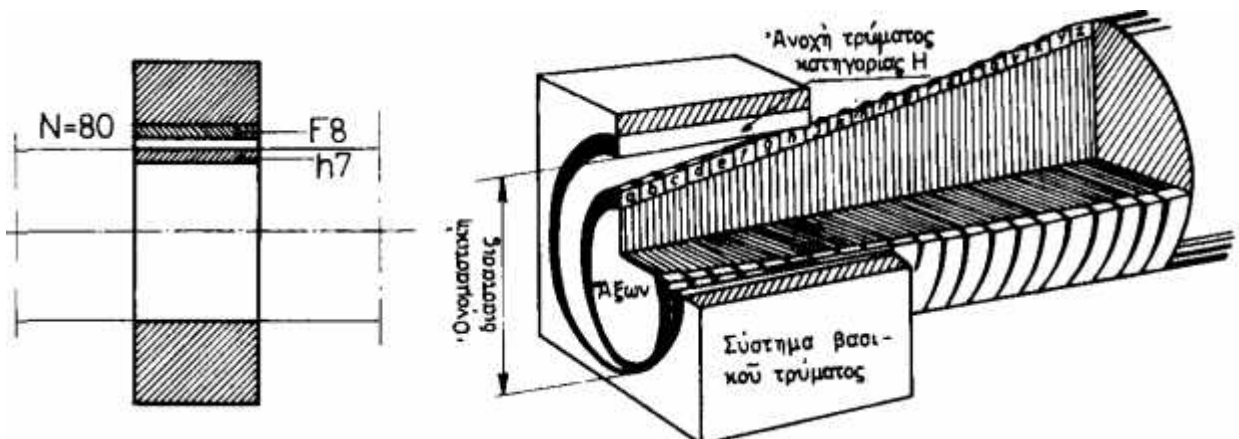
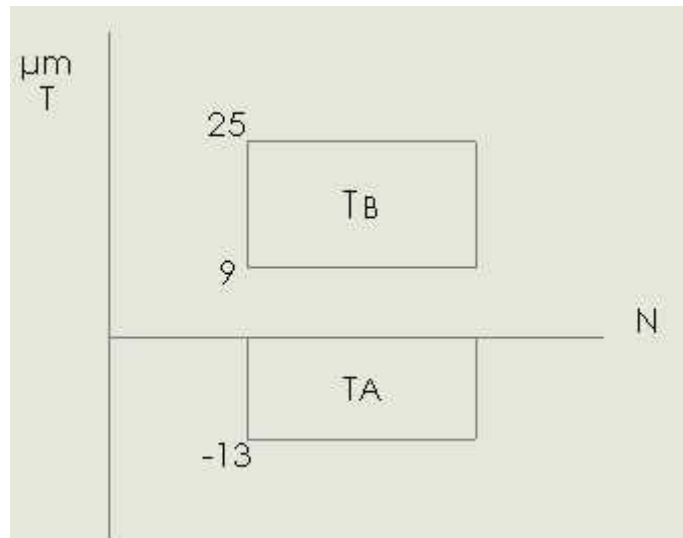
$$X_{\varepsilon} = E_{\varepsilon} - A_{\mu} = 42,009 - 42,000 = 0,009\text{mm}$$

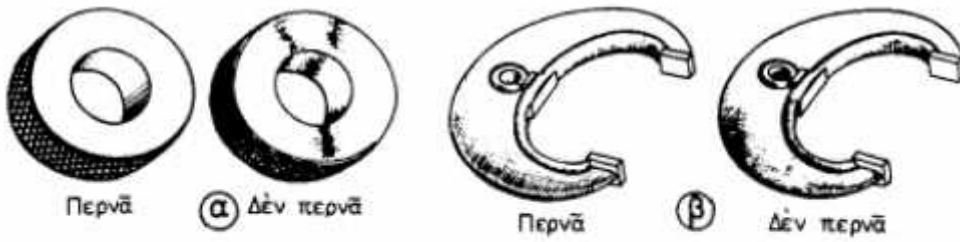
μ

μ .

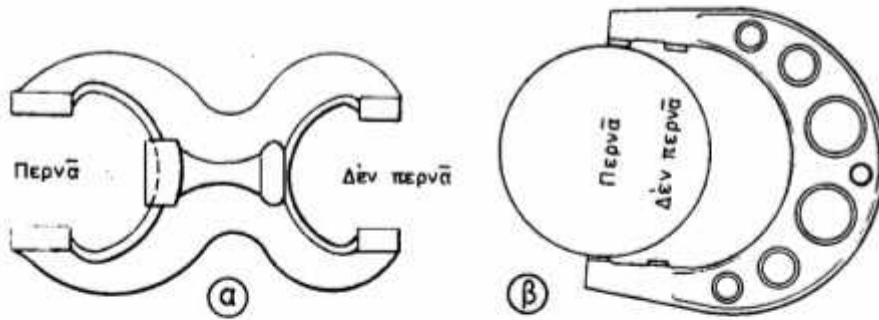
μ

μ μ :

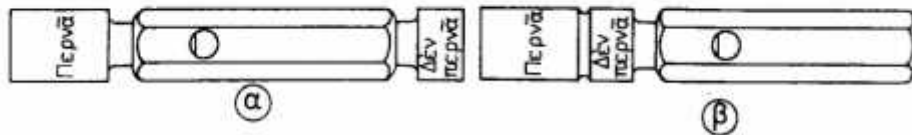




Ελεγκτήρες: (α) Δακτυλίδια. (β) Σε σχήμα πετάλου



Ελεγκτήρες: (α) Σε σχήμα διτλού πετάλου. (β) με διτλό επαφέα.



Κυλινδρικοί ελεγκτήρες ελέγχου τρυμάτων

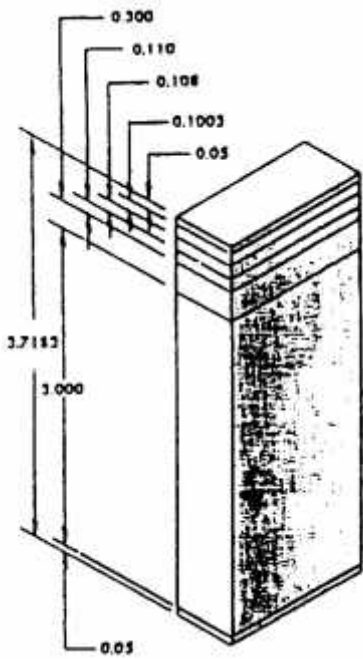
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 49,950mm(). μ μ μ μ μ
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 , μ μ μ , μ
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 $\mu\mu$
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 (μ)).
 μ μ .

3.6.4.1.

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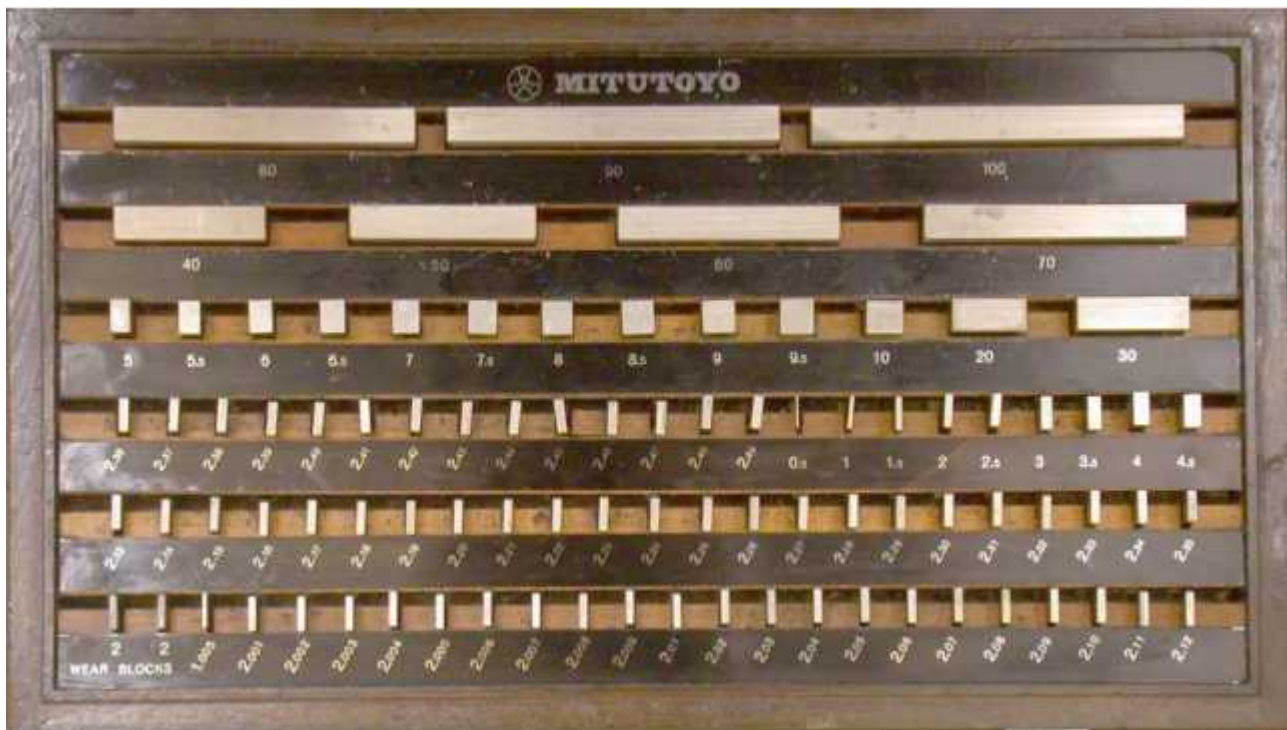
- ❖ μ .
- ❖ μ .
- ❖ μ .
- ❖ μ μ.
- ❖ « » « »



-
- μ μ
 - 1 x 0.10031
 - 1x0.108
 - 1x0.11
 - 2x0.05=0.1
 - 1x0.3
 - 1x3.0
-

3.7183 inches

μ 4.1.



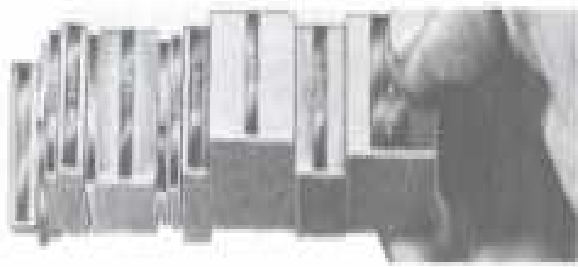
4.2.:

μ , μ μ μ

μ	μ	μ	μ (μm)	μ (μm)
81	86	9 49 19 4	2542,5-2562,9 2565,4-3784,6 1270-24130 $25400 - 1,0160 \cdot 10^5$	2,5400 25,400 1270 25400
36 μ	36	9 9 9 1 5 2 1	2542,5-2562,2 2565,4-2768,6 2794-4826 1270 2540-12700 25400-50800 $1,0160 \cdot 10^5$	2,5400 25,400 254 1270 2540 25400 $1,0160 \cdot 10^5$
28	28	1 9 9 9	509,27 510,54-530,86 533,4-736,6 254-2286	0,00005 0,0001 0,001 0,010
21	21	1 9 11	255,27 256,54-276,86 254-508	0,00005 0,0001 0,001
8 μ	8	4 2 2	$1,2700 \cdot 10^5$ - $2,0320 \cdot 10^5$ $5,5400 \cdot 10^5$ - $3,0480$ $\cdot 10^5$ $4,0640 \cdot 10^5$ - $5,0800 \cdot 10^5$	1,00 2,00 4,00

4.4.: μ μ μ .

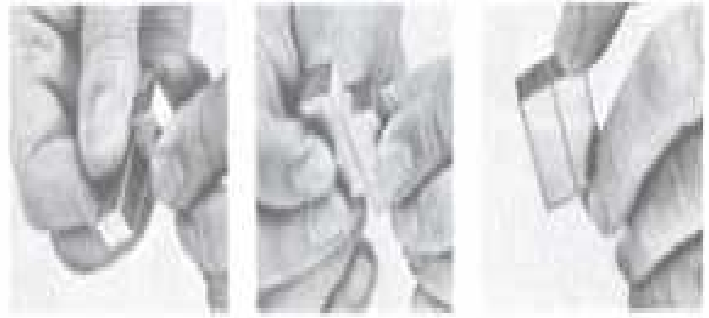
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 μ μ μ μ μ .
 μ μ μ , μ , μ μ .
 μ μ μ μ μ μ .
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 μ μ
(.3.3. . 3.4).



Pratt & Whitney Cutting Tool and Gage Div., Colt Industries

μ 4.3.:

μ μ



CEJ Gage Company

μ 4.4:

4.7.

μ

μ

μ

μ

ANSI B89.1.9 M-

1984 (R1989).

μm

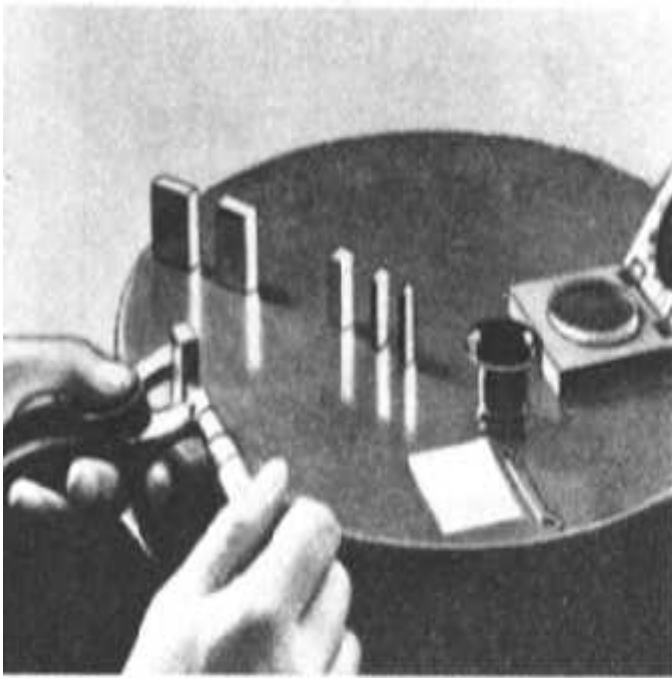
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μ

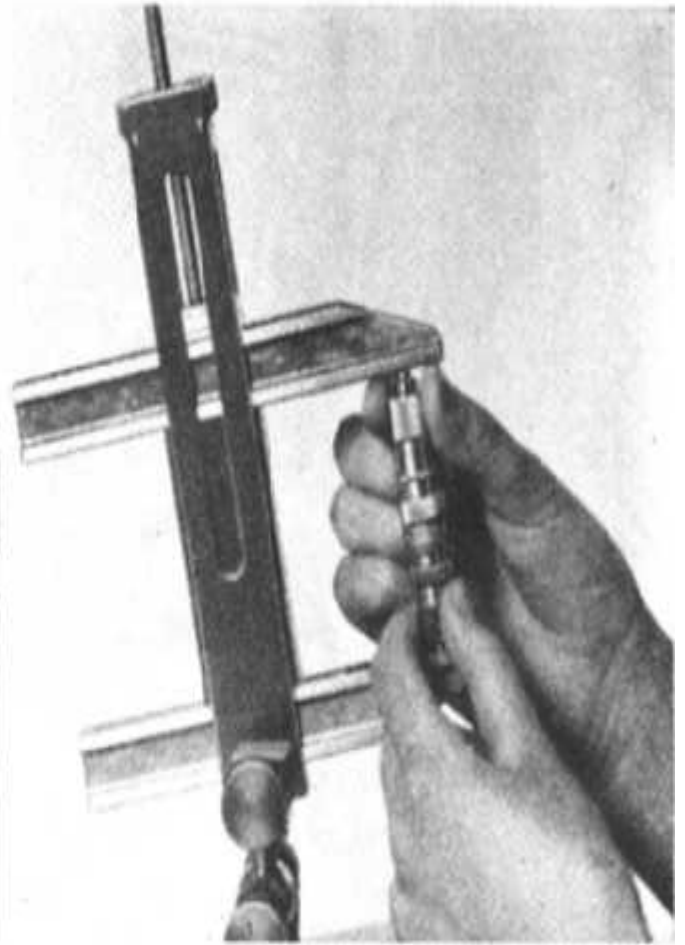
μ

DIN 861.

(mm)	0			
0,1	-	0,2	0,5	1,0
0,5	0,1	0,2	0,5	1,0
10	0,12	0,25	0,6	1,2
20	0,14	0,3	0,7	1,4
30	0,16	0,35	0,8	1,6
40	0,18	0,4	0,9	1,8
50	0,2	0,45	1,0	2,0
60	0,22	0,5	1,1	2,2
70	0,24	0,55	1,2	2,4
80	0,26	0,6	1,3	2,6
90	0,28	0,65	1,4	2,8
100	0,3	0,7	1,5	3
150	0,4	0,95	2,0	4
200	0,5	1,2	2,5	5
300	0,7	1,7	3,5	7
400	0,9	2,2	4,5	9
500	1,1	2,7	5,5	11
600	1,3	3,2	6,5	13
700	1,5	3,7	7,5	15



4.9.: μ μ μ
μ .

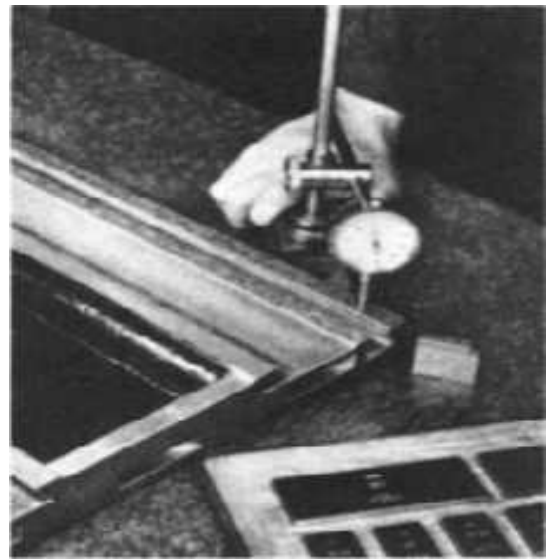


4.10.: μ μ μ
μ .



Brown & Sharpe Mfg. Co.

4.11.: μ μ μ μ .

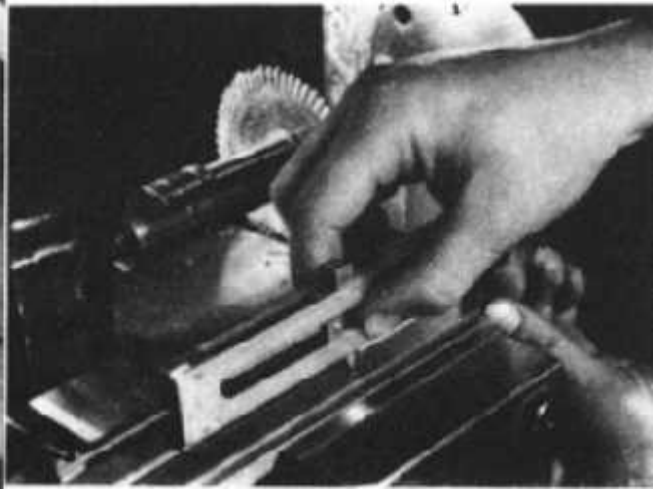


4.12.: μ

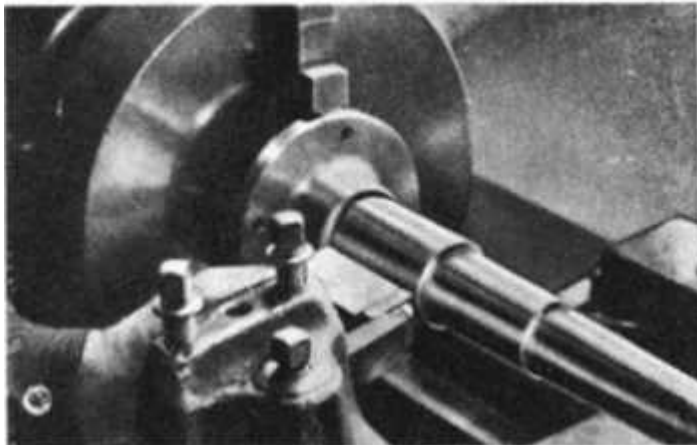
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(: - μ μ ,
http://dspace.lib.ntua.gr/bitstream/123456789/3861/3/papadopoulostd_metrology.pdf).

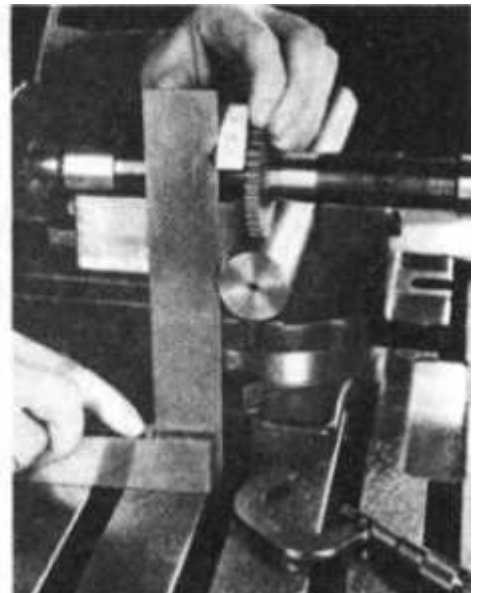


4.13:



4.14: μ

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4.15: μ

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4.10.

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5.1.2.

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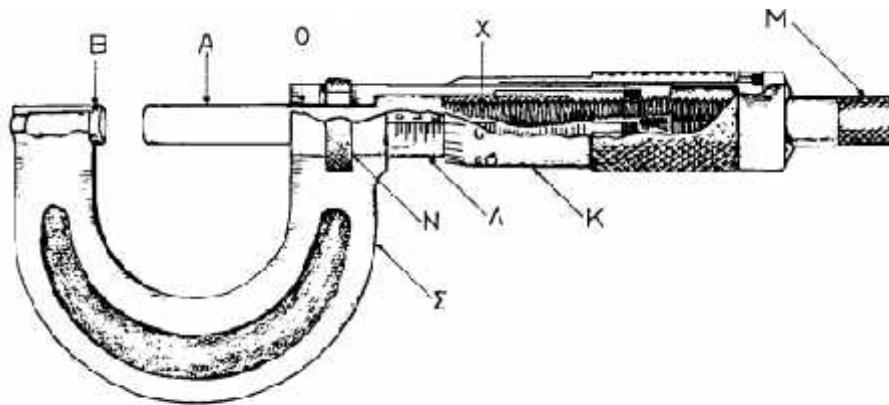
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$\mu \quad \mu \quad \mu$

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 μ 0,5mm.
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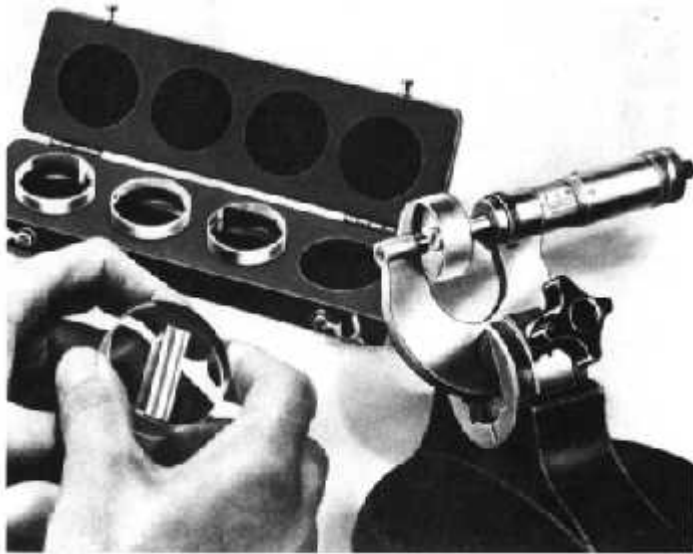
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μ =±0,15μ.



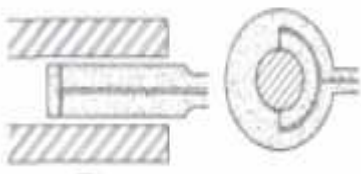
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=±0,75μ.

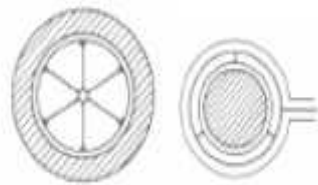
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5.4.() .

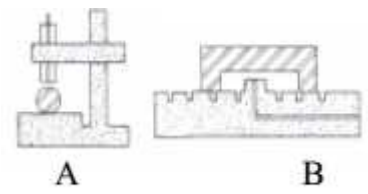
5.4.() .



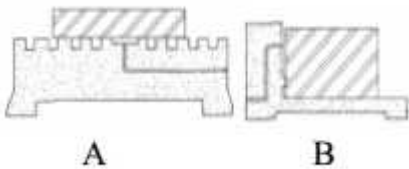
5.4.()



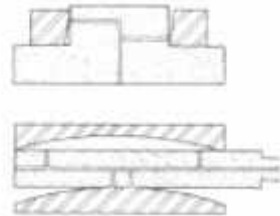
5.4.()



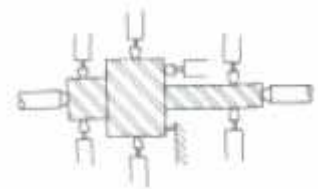
5.4.()



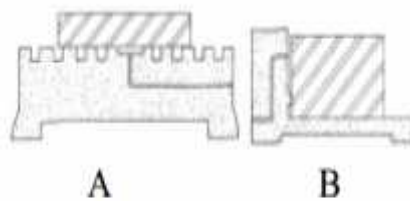
5.4.()



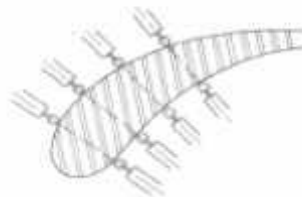
5.4.()



5.4.()



5.4.()



5.4.()

5.3.5.

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software

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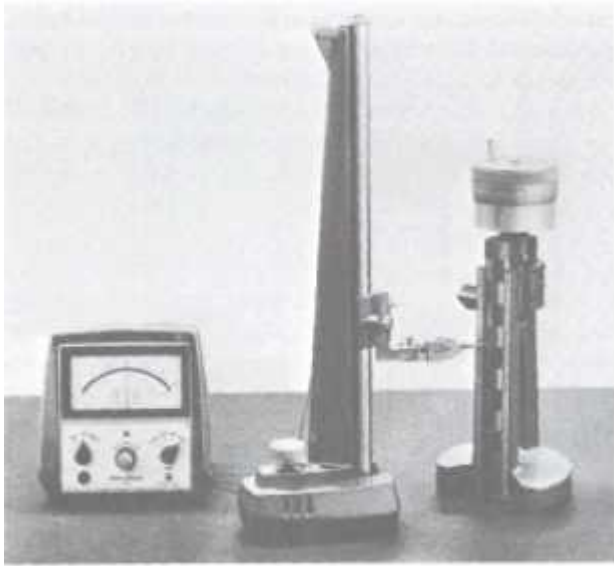
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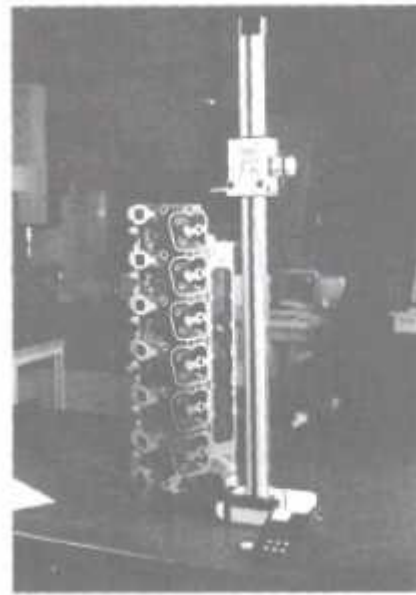
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(.5.5.)



Brown & Sharpe Mfg. Co.



Mahr-Gage Co.

5.11.:

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5.12.:

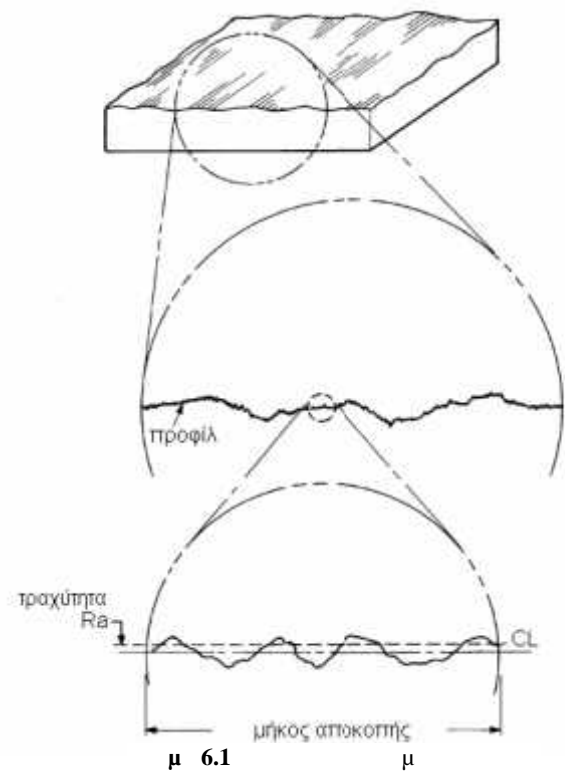
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5.4.3.

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6.1.



6.2.

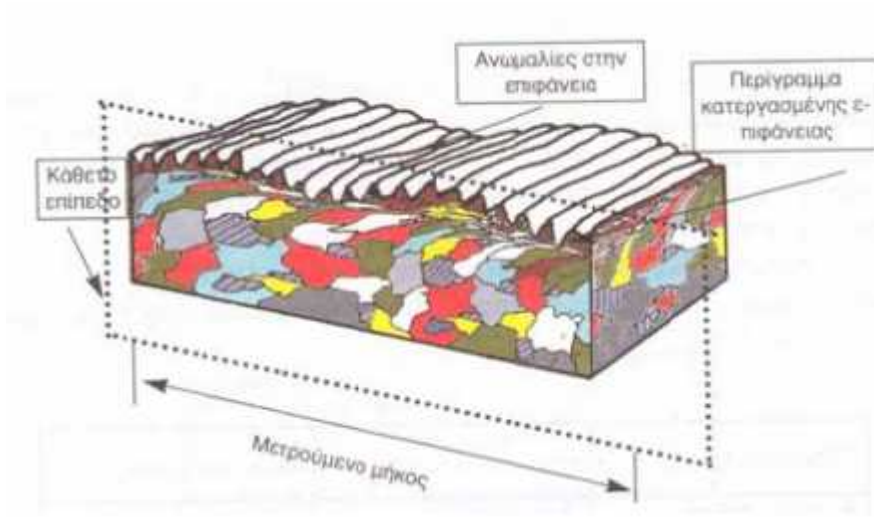
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6.3.

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μ 6.3

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6.4.3

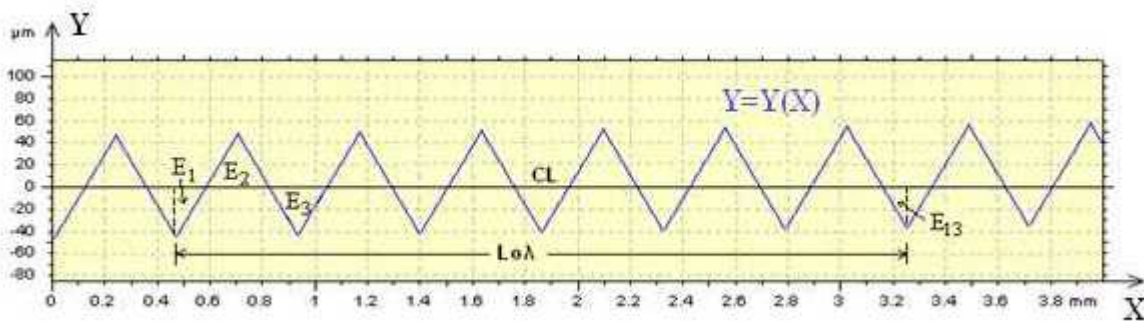
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$\mu \mu \mu$
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$$R_a = \frac{1}{L} \int_0^L |y| dx \quad (4.2)$$

$\mu \mu \mu \mu$ (
) $\mu \mu$. μ
 $\mu \mu \mu \mu \mu$.
 μ , $\mu \mu \mu$,
 μ 4.9. μ :

$$R_a = \frac{E_{o\lambda}}{L_{o\lambda}} = \frac{E_1 + E_2 + \dots + E_{13}}{L_{o\lambda}} \quad (4.3)$$



μ 6.10 $\mu \mu \mu \mu \mu \mu$

6.4.4.

$\mu \mu$ μ **Rt**

$\mu \mu \mu \mu$. $\mu \mu$
 $\mu \mu \mu \mu$.

R_t/R_{max}		$R_t = R_p + R_v$
R_{ti}		$R_{ti} = R_{pi} + R_{vi}$
R_{tm}	μ	$R_{tm} = \frac{1}{n} \sum_{i=1}^n R_{ti}$
R_y		$R_y = \max_i R_{ti}$
R_{3y}	μ	$R_{3y} = \frac{1}{5} \left(\sum_{i=1}^5 R_{3yi} \right)$
k		$k = \frac{R_v}{R_{max}}$
R_{sk}	$\mu\mu$	$R_{sk} = \frac{1}{R_q^3} \int_{-\infty}^{+\infty} y^3 p y dy$ $R_{sk} = \frac{1}{NR_q^3} \left(\sum_{i=1}^N Y_i^3 \right)$
R_{ku}		$R_{ku} = \frac{1}{R_q^4} \int_{-\infty}^{+\infty} y^4 p y dy$ $R_{ku} = \frac{1}{NR_q^4} \left(\sum_{i=1}^N Y_i^4 \right)$

6.2.:

 μ μ

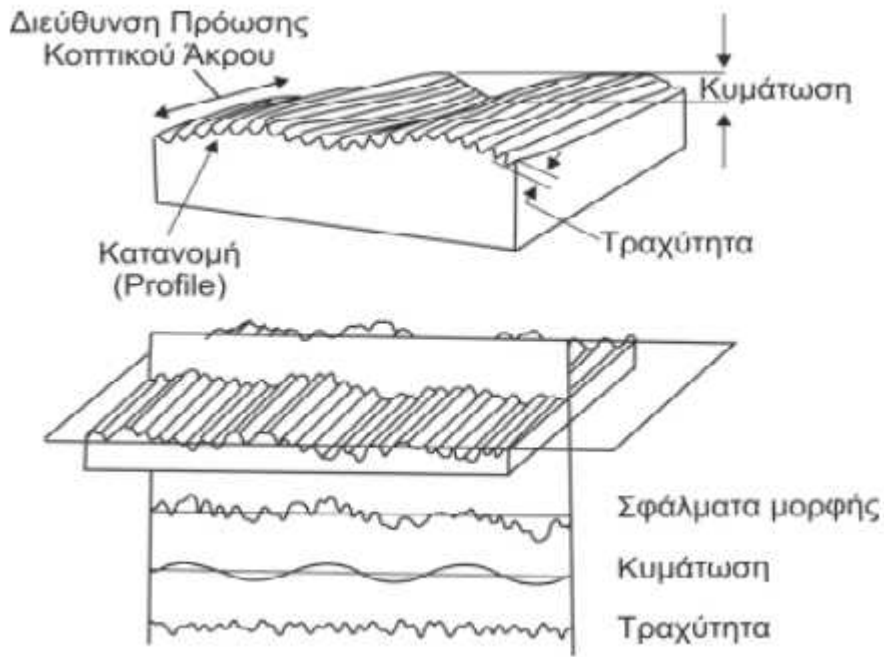
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2	μ / μ μ	μ μ μ . μ . μ . μ . μ .
3		μ μ .
4	μ . μ . μ . .	μ μ . μ . μ . μ . μ .
5		μ μ μ . μ .
6	μ μ μ	μ - μ μ . μ μ μ μ

6.4.:

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μ 6.14: () μ μ ()

πρώτης τάξεως (σχ. 4.1.5α)



Σχήμα 4.1.5α

δευτέρας τάξεως (σχ. 4.1.5β)



Σχήμα 4.1.5β

τρίτης τάξεως (σχ. 4.1.5γ)



Σχήμα 4.1.5γ

τετάρτης τάξεως (σχ. 4.1.5δ)



Σχήμα 4.1.5δ

πέμπτης τάξεως (σχ. 4.1.5ε)



Σχήμα 4.1.5ε

- μ . , $\mu \mu$
- μ . μ , $\mu \mu$.
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6.6.2.

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$\mu \mu \mu \mu \mu \mu$ (pick-ups).
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2. .

μ 6.18.

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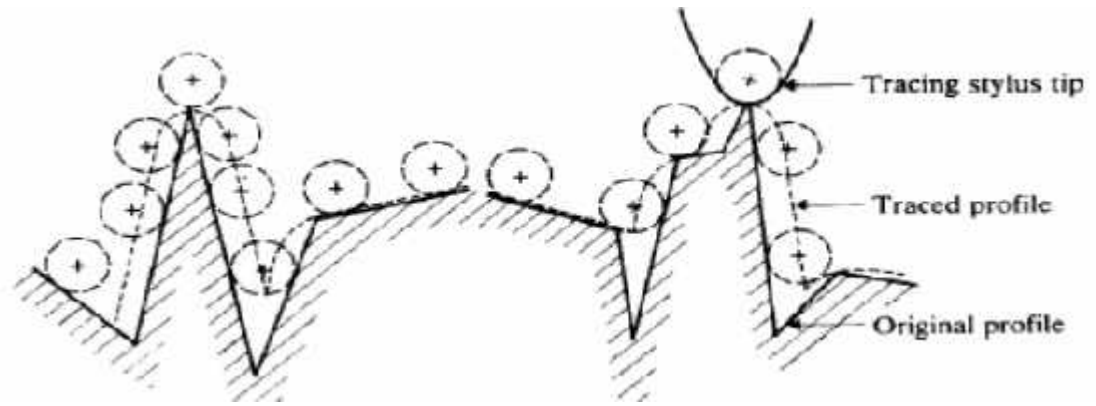
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. $\mu \mu$

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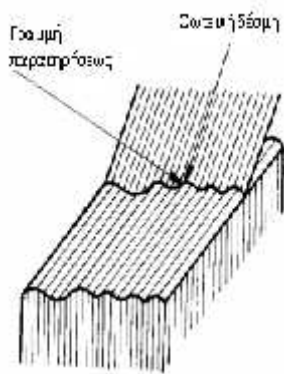
, μ .



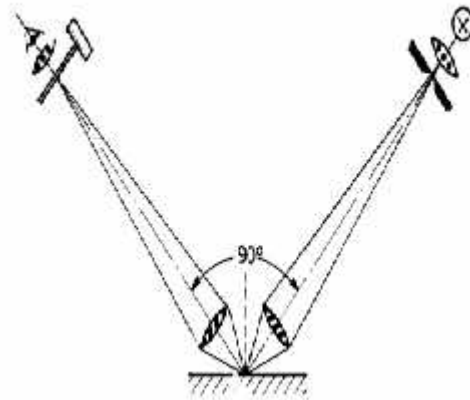


μ 6.18

- **Schmaiz.** μ μ μ , μ
 μ μ μ 45 . μ μ , μ μ
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μ 6.20



μ 6.21



μ 6.22



μ 6.25 T μ Surtronic 3+

6.7. μ μ

- μ μ (Ö). μ (140 2/1931), μ μ

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6.5: μ μ

- μ $\mu\mu$ μ « » .

DIN 3141/1960 DIN 150 1302, μ μ μ $\mu\mu$
 μ μ μ .

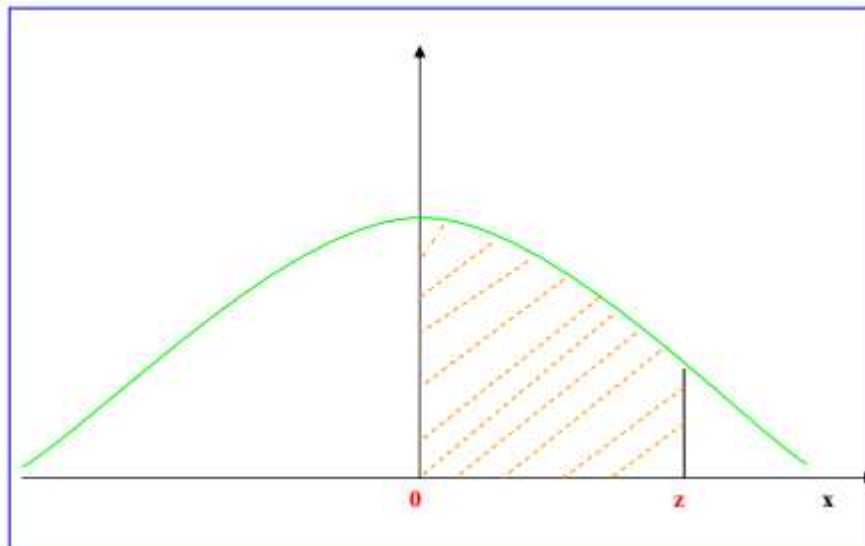
ΛΕΙΟΤΗΤΑ ΕΠΙΦΑΝΕΙΑΣ.	Βοθμός λείανσης R σε μm.	
ΕΙΔΟΣ ΚΑΤΕΡΤΑΣΙΑΣ.	▽	
	▽▽▽▽	▽▽
	0,1 0,16 0,25 0,40	0,63 1,0 1,6 2,5 4,0 6,3 10 16 25 40 63 100 160 250 400 630 1000
ΑΜΜΟΚΥΤΟ		
ΛΕΠΤΟΚΥΤΟ		
ΕΙΛΗΡΟΥΡΤΙΚΗ ΔΙΑΜΟΡΦΩΣΗ		
ΚΥΛΙΝΔΡΑΡΙΣΜΑ		
ΕΞΕΛΑΣΗ		
ΠΡΕΖΑΡΙΣΜΑ		
ΛΙΜΑΡΙΣΜΑ χονδρό		
ΛΙΜΑΡΙΣΜΑ λείανσης		
ΠΡΑΝΙΣΜΑ χονδρό		
ΠΡΑΝΙΣΜΑ λείανσης		
ΤΟΡΝΙΡΙΣΜΑ χονδρό		
ΤΟΡΝΙΡΙΣΜΑ λείανσης		
ΤΟΡΝΙΡΙΣΜΑ με σκληρομέταλλο		
ΤΟΡΝΙΡΙΣΜΑ με διαμάντι		
ΤΡΙΒΗ		
ΤΡΙΒΗ λεία		
ΦΡΕΖΑΡΙΣΜΑ λείανσης		
ΦΡΕΖΑΡΙΣΜΑ λείανσης ποιότητας		
ΕΥΣΙΜΟ		
ΑΚΟΝΙΣΗ		
ΑΚΟΝΙΣΗ ποιότητας		
ΑΚΟΝΙΣΗ με εξέλαση		
ΕΤΙΛΒΩΣΗ		
ΕΤΙΛΒΩΣΗ ποιότητας		
ΓΥΑΛΙΣΜΑ		
ΑΜΟΡΦΙΠΗ ακόνιση υψηλής ποιότητας		

6.26:

μ

μ

μ



μ 7.4.

z	0.00	0.01	0.02	0.03	0.04	0.05	0.06	0.07	0.08	0.09
.0	.5000	.5040	.5080	.5120	.5160	.5199	.5239	.5279	.5319	.5359
.1	.5398	.5438	.5478	.5517	.5557	.5596	.5636	.5675	.5714	.5753
.2	.5793	.5832	.5871	.5910	.5948	.5987	.6026	.6064	.6103	.6141
.3	.6179	.6217	.6255	.6293	.6331	.6368	.6406	.6443	.6480	.6517
.4	.6554	.6591	.6628	.6664	.6700	.6736	.6772	.6808	.6844	.6879
.5	.6915	.6950	.6985	.7019	.7054	.7088	.7123	.7157	.7190	.7224
.6	.7257	.7291	.7324	.7357	.7389	.7422	.7454	.7486	.7517	.7549
.7	.7580	.7611	.7642	.7673	.7703	.7734	.7764	.7794	.7823	.7852
.8	.7881	.7910	.7939	.7967	.7995	.8023	.8051	.8078	.8106	.8133
.9	.8159	.8186	.8212	.8238	.8264	.8289	.8315	.8340	.8365	.8389
1.0	.8413	.8438	.8461	.8485	.8508	.8531	.8554	.8577	.8599	.8621
1.1	.8643	.8665	.8686	.8708	.8729	.8749	.8770	.8790	.8810	.8830
1.2	.8849	.8869	.8888	.8907	.8925	.8944	.8962	.8980	.8997	.9015
1.3	.9032	.9049	.9066	.9082	.9099	.9115	.9131	.9147	.9162	.9177
1.4	.9192	.9207	.9222	.9236	.9251	.9265	.9279	.9292	.9306	.9319
1.5	.9332	.9345	.9357	.9370	.9382	.9394	.9406	.9418	.9429	.9441
1.6	.9452	.9463	.9474	.9484	.9495	.9505	.9515	.9525	.9535	.9545
1.7	.9554	.9564	.9573	.9582	.9591	.9599	.9608	.9616	.9625	.9633
1.8	.9641	.9649	.9656	.9664	.9671	.9678	.9686	.9693	.9699	.9706
1.9	.9713	.9719	.9726	.9732	.9738	.9744	.9750	.9756	.9761	.9767
2.0	.9772	.9778	.9783	.9788	.9793	.9798	.9803	.9808	.9812	.9817
2.1	.9821	.9826	.9830	.9834	.9838	.9842	.9846	.9850	.9854	.9857
2.2	.9861	.9864	.9868	.9871	.9875	.9878	.9881	.9884	.9887	.9890
2.3	.9893	.9896	.9898	.9901	.9904	.9906	.9909	.9911	.9913	.9916
2.4	.9918	.9920	.9922	.9925	.9927	.9929	.9931	.9932	.9934	.9936
2.5	.9938	.9940	.9941	.9943	.9945	.9946	.9948	.9949	.9951	.9952

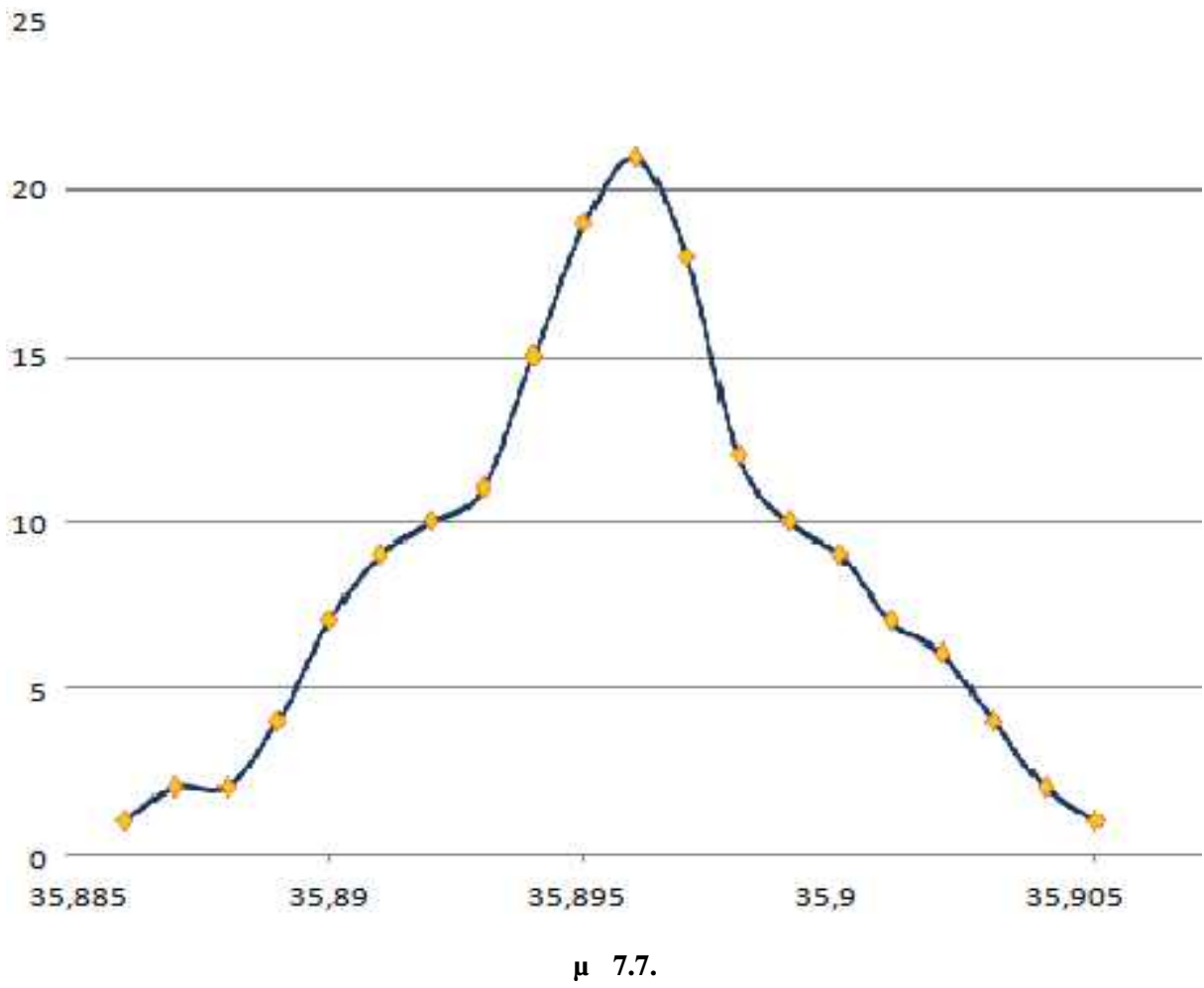
$$P(z \in [0, 1.46]) = P(0 \leq z \leq 1.46) = 0.9279 - 0.006 = 0.9219.$$

$$P(z < 1.46) = P(z \leq 1.46) - P(z = 1.46) = 0.9279 - 0 = 0.9279.$$

$$P(z = 1.46) = 0 \quad P(z = 0) = 0.$$

$$P(0 < z < 1.46) = P(0 < z < 1.46) = 0.9279 - 0 = 0.9279,$$

$$P(z = 1.46) = 0 \quad P(z = 0) = 0.$$



μ μ μ μ μ μ

X_m, x_i, x_i^2, m, q . μ μ

/	Xi	xi		xi ²
		+	-	
1	35,891		8	64
2	35,892		7	49
3	35,893		6	36
4	35,895		4	16
5	35,897		2	4
6	35,898		1	1
7	35,9	1		1
8	35,903	4		16
9	35,906	7		49
10	35,909	10		100
11	35,911	12		144
12	35,909	10		100
13	35,906	7		49
14	35,903	4		16
15	35,9	1		1
16	35,898		1	1
17	35,896		3	9
18	35,894		5	25
19	35,892		7	49
20	35,891		8	64
	717,984	56	52	794

$$\mu = \frac{\sum |xi|}{N} = \frac{717,984}{20} = 35,899$$

$$X_1 = 35,891 - 35,899 = -0,008 \text{ mm} = -8 \mu\text{m}$$

$$\mu = \dots$$

$$: m = \frac{\sum |xi|}{N*(N-1)} = \frac{56+52}{\sqrt{20*19}} = 5,54$$

$$: q = \frac{\overline{\sum xi^2}}{N-1} = \frac{794}{19} = 6,5$$

$$\mu = \dots$$

$$\varepsilon_m = 0,845 * m = 4,6 \mu\text{m}$$

$$\varepsilon_q = 0,675 * q = 4,3 \mu\text{m}$$

$$\varepsilon = \frac{\varepsilon_m + \varepsilon_q}{2} = 4,45 = 4 \mu\text{m}$$

	μ	μ	μ :
•	35,890	35,905	80%
•		35,910	3%
•	35,890	8%	.

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